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► To cite this version:

Daniel Delahaye, Adrían García, Julien Lavandier, Supatcha Chaimatanan, Manuel Soler. Air Traffic Complexity Map Based on Linear Dynamical Systems. Aerospace, 2022, 10.3390/aerospace9050230 . hal-03647918

HAL Id: hal-03647918 https://enac.hal.science/hal-03647918

Submitted on 21 Apr 2022

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Article Air Traffic Complexity Map Based on Linear Dynamical Systems

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Abstract: This paper presents a new air traffic complexity metric based on linear dynamical systems, of which the goal is to quantify the intrinsic complexity of a set of aircraft trajectories. Previous works 2 have shown that the structure and organization of air traffic are essential factors in the perception of the complexity of an air traffic situation. Usually they were not able to explicitly address trajectory 4 pattern organization. The new metric, by identifying the organization properties of trajectories in 5 a traffic pattern, captures some of the key factors involved in ATC complexity. The key idea of this work is to find a linear dynamical system which fits a vector field as closely as possible to 7 the observations given by the aircraft positions and speeds. This approach produces an aggregate 8 complexity metric that enables to identify high (low) complexity regions of airspace and compare 9 their relative complexity. The metric is very appropriate to compare different traffic situations for any 10 scale (sector or country) by associatting a complexity index to each trajectory sample in the airspace. 11 For instance, to compute the complexity for a sector, one must just sum-up complexity for trajectory 12 samples intersecting such a sector. This computation can also be extended in the time dimension in 13 order to estimate the average complexity in a given airspace for a period of time. 14

Keywords: Complexity; Dynamical System; Air Traffic Disorder

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1. Introduction

Regarding air traffic management research, there have been three main objectives of interest: reduce air flight delay, solve air traffic conflicts efficiently and mitigate air space congestion. This work proposes a method to assess the latter.

The operational capacity of a control sector is measured by the maximum number of 20 flights that may cross the sector in a given period. This measurement does not consider 21 the direction of the traffic, treating geometrically structured and disordered traffic in the 22 same way. Thus, in certain situations, a controller may continue to accept traffic even 23 if operational capacity has been reached (structured traffic situation). In other cases, a 24 controller may need to refuse airplanes even though the operational capacity has not 25 been reached (disordered traffic situation). Thus, modeling airspace congestion using the 26 number of airplanes per unit of time is insufficient to reflect the levels of difficulty involved 27 in a traffic situation. 28

Air traffic control organizes air flows to ensure flight safety and increase the route 29 network's capacity. In 2019, before COVID, about 8500 flights were registered everyday 30 over France, which is a crossroad for the whole European airspace. This traffic generates a 31 huge amount of control workload, and the airspace is then divided into elementary sectors 32 which air navigation controllers manage. For several years, a constant increase in air traffic 33 has induced more and more congestion in the control sectors. Two strategies can then be 34 applied to reduce such congestion. The first one consists of adapting the demand to the 35 existing capacity (slot-route allocation, collaborative decision-making, etc...). The second 36 one adapts the capacity to the demand (modification of the air network, new design of 37 the sectorization, new airports, etc...). For the two preceding approaches, the capacity of a 38

Citation: Delahaye, D.; García, A; Lavandier, J.; Chaimatanan, S.; Soler, M. Title. *Aerospace* **2022**, *1*, 0. https://doi.org/

Received: Accepted: Published:

Publisher's Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.

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Version April 21, 2022 submitted to Aerospace

sector is measured by the number of aircraft flying across the sector during a given period of time.

This study aims to synthesize a traffic complexity indicator to quantify better the 41 congestion in the air sector, which will be more relevant than a simple number of aircraft 42 independent of the traffic configuration. More precisely, our objective is to build a metric 43 of the intrinsic complexity of the traffic distribution in the airspace, which relates to 44 controller workload. Such metrics must capture the level of disorder (or organization) of 45 any traffic distribution. Usually, metrics are focused on the speed vector distribution, and 46 the associated disorder metric captures only some features of the traffic complexity. The 47 real objective of our work is to build a metric that measures the disorder or organization of 48 trajectories in 4D space (3D for space and 1D for time). 49

Such complexity metrics are relevant for many applications in the air traffic man-50 agement area. For instance, when a sectorization is designed[1], the sectors have to be 51 balanced from the congestion point of view and nowadays, only the number of aircraft is 52 used to reach this objective. Another example where a congestion metric is needed is the 53 traffic assignment [2,3] for which an optimal time of departure and a route are searched for each aircraft in order to reduce the congestion in the airspace. Complexity metric may 55 also be used to design new air networks, for dynamic sectoring concepts, define future 56 ATM concepts (Free Flight), etc... Complexity metrics enable to qualify and quantify the 57 performance of the Air Traffic service providers and enable a more objective consultation 58 between airlines and providers. 59

The work presented in this paper is based on dynamical systems modeling of air 60 traffic. A dynamical system describes the evolution of a given state vector. If such a vector 61 is given by the position of aircraft $\vec{X} = [x, y, z]^T$, a dynamical system associates a speed 62 vector $\vec{X} = [v_x, v_y, v_z]^T$ to each point in the airspace. The key idea is to find a dynamical 63 system that models the observed aircraft trajectories. A trajectory disorder metric can be 64 computed based on this dynamical system modeling. The metric is targeted to measure the 65 intrinsic traffic complexity related to a set of 4D trajectories related to the control workload. Such control workload encompasses other factors (airspace structure, etc...) that are not 67 considered in the metric computation.

In the first part, this paper will summarize the previous related works. The second part will present a linear dynamical system modeling for which the complexity metric can be represented into a complex coordinate system. It is very easy to identify any speed vector organization pattern in this system. The third part illustrates the computation of such a metric in several traffic situations.

2. Previous Related Works

The airspace complexity is related to the traffic structure and the airspace geometry. Different efforts are underway to measure the whole complexity of the airspace.

Wyndemere Inc. [4] proposed a measure of the perceived complexity of an air traffic situation. This measure is related to the controller's cognitive workload with or without knowing the aircraft's intents. The metric is human-oriented and is then very subjective.

Laudeman et al. from NASA [5] have developed a metric called "Dynamic Density" 80 which is more quantitative than the previous ones and is based on the flow characteristics 81 of the airspace. The "Dynamic Density" is a weighted sum of the traffic density (number 82 of aircraft), the number of heading changes (>15 degrees), the number of speed changes 83 (>0.02 Mach), the number of altitude changes (>750 ft), the number of aircraft with 3D 84 Euclidean distance between 0 - 25 nautical miles, the number of conflicts predicted in 85 25-40 nautical miles. The parameters of the sums have been adjusted by showing different traffic situations to several controllers. B. Sridhar from NASA[6] has developed a model 87 to predict the evolution of such a metric in the near future. Efforts to define "Dynamic 88 Density" have identified the importance of many potential complexity factors, including 89 structural considerations. 90

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Airspace complexity depends on both structural and flow characteristics of the airspace[6]. The structural characteristics are fixed for a sector and depend on the spatial and physical attributes of the sector, such as terrain, number of airways, airway crossings, and navigation aids. The flow characteristics vary as a function of time and depend on the number of aircraft, the mix of aircraft, weather, the separation between aircraft, etc... A combination of these structural and flow parameters influences the controller workload.

The traffic itself is not enough to describe the complexity associated with an airspace. 97 A few previous studies have attempted to include structural consideration in complexity 98 metrics but have done so only to a restricted degree. For example, the Wyndemere Corpo-99 ration proposed a metric that included a term based on the relationship between aircraft 100 headings and dominant geometric axis in a sector [4]. The importance of including struc-101 tural consideration has been explicitly identified in recent work at Eurocontrol. In a study 102 to identify complexity factors using judgment analysis, "Airspace Design" was identified 103 as the second most crucial factor behind traffic volume[7]. The impact of the structure on the controller workload can be found on the paper[8,9]. Those papers show how strong the 105 traffic structure (airways, sectors, etc...) is related to the control workload through several 100 traffic factors dependent on the instantaneous distribution of traffic (clustering, number of 107 aircraft, distance between aircraft, relative speed between aircraft, etc...)

The previous models do not take into account the intrinsic traffic disorder, which is 109 related to the complexity. The first efforts related to disorder can be found in[10]. This paper introduces metrics based on geometrical properties that measure a traffic pattern's disorder. 111 Those metrics can extract features on the traffic complexity such as proximity (measures 112 the level of aggregation of aircraft in the airspace), convergence (for close aircraft, this 113 metric measures how strongly aircraft are closer to each other), and sensitivity (this metric 114 measures how the relative distance between aircraft is sensible to the control maneuver). G. 115 Aigoin has extended and refined the geometrical class by using a cluster-based analysis[11]. 116 Two aircraft are said to be in the same cluster if the product of their relative speed and 117 their proximity (a function of the inverse of the relative distance) is above a threshold. 118 For each cluster, a metric of relative dependence between aircraft is computed, and the 119 whole complexity of the cluster is then given by a weighted sum of the matrix norm. Those 120 norms give an aggregated measure of the level of proximity of aircraft in clusters and the 121 associated convergence. From the cluster matrix, it is also possible to compute the difficulty 122 of a cluster (it measures how hard it is to solve a cluster). Multiple clusters can exist within a sector, and their interactions must also be considered. A measure of this interaction has 124 been proposed by G. Aigoin [11]. This technique allows multiple complexity metrics to be developed, such as average complexity, maximum and minimum cluster complexities, and 126 complexity speeds. 127

Another approach based on fractal dimension has been proposed by S. Mondoloni and 128 D. Liang in[12]. Fractal dimension is a metric comparing traffic configurations resulting 129 from various operational concepts. It allows, in particular, to separate the complexity 130 due to sectorization from the complexity due to traffic flow features. The dimension of 131 geometrical figures is well-known: a line is of dimension 1, a rectangle of dimension 2, 132 etc. The application of this concept to air route analysis consists in computing the fractal 133 dimension of the geometrical figure composed of existing air routes. Fractal dimension 134 provides information on the number of degrees of freedom used in the airspace: a higher 135 fractal dimension indicates more degrees of freedom. Therefore, the fractal dimension 136 measures the geometrical complexity of a traffic pattern. 137

Some new geometrical metrics have been developed in [13] which are able to capture the level of disorder or the level of organization for some traffic patterns. For instance, in an artificial roundabout moving, the speed vectors are very different even if the global for some traffic patterns are speed vectors are very different even if the global for some traffic patterns. For instance, in first organized without any changes in the relative distance between aircraft. The covariance and the Koenig metrics have been developed to capture those features. The first one is able to identify the disorder or organization of translation movements. The second one identifies organized curl moving.

In[10] another approach based on nonlinear dynamical system modeling of the air 145 traffic uses the topological entropy as a measure of the disorder of the traffic pattern. This 146 approach represents more faithfully the traffic's structure but requires a lot of computation 147 for establishing the metric. First, the non-linear dynamical system is adjusted to the 148 observations in order to build the associated vector field. Then, Lyapunov exponents 149 are computed in order to characterize the overall properties of the vector field. When an 150 exponent has a high value, it shows a high sensitivity to initial conditions meaning the 151 situation is difficult to predict. In this case the traffic situation presents a high level of 152 disorder. Unfortunately, this metric is not able to take uncertainties into account which is 153 the case when one want to predict congestion in the near future. 154

We propose in this paper an approximation of such a metric based on the linear dynamical system, which measures the local disorder of a set of trajectories in the neighborhood of a given aircraft at a given time. This approximation is much faster to compute and can take into account uncertainties of the future position of aircraft, which is not possible with the nonlinear dynamical system framework described in[10].

3. Metric Description (Linear Dynamical System Modeling)

The investigated indicator will be linked to the air traffic modeling by a linear dynamical system, yielding an intrinsic measure of complexity of the geometry of the traffic. This enables to identify different structures of organization of the aircraft speed vectors such as translation, curve organizations, divergence, convergence, or a mix of them.

3.1. Model

The key idea of this metric is to model the set of aircraft trajectories by a linear dynamical system. A dynamical system models a vector field by a set of differential equations which describes and controls the evolution of a given state vector and is defined by the following equation:

$$\vec{X} = \mathbf{A} \cdot \vec{X} + \vec{B} \tag{1}$$

 \vec{X} is the state vector of the system:

$$\vec{X} = \begin{bmatrix} x \\ y \end{bmatrix}$$
(2)

In this equation, we only consider the observations' x and y components since air traffic controllers see two dimensions speed vectors on their screens. Moreover, the metric will be computed for each flight level in a given airspace. Equation 1 associates a speed vector \vec{X} with each point in the state space \vec{X} . This synthesis is a particular vector field. The average behavior of this vector field is given by the vector \vec{B} and the linear mapping between the speed vector \vec{X} and the position vector \vec{X} is given by matrix **A**. Therefore, the coefficients of matrix **A** and vector \vec{B} determine the mode of evolution of the system in relation to its dynamics.

More precisely, the eigenvalues of this matrix will determine the behavior of the system and will be used to obtain the complexity metric. The properties and relevance of these eigenvalues will be explained in section 3.3.

First, we focus on defining and modeling the linear dynamical system that will allow us to obtain matrix **A**. Our problem therefore consists on determining the dynamical model which is closest to the observations: Those observation are extracted from the radar trackers (positions and speeds of aircraft at a given time). We then consider that for each aircraft, we have set position \vec{X}_i and speed measures \vec{V}_i at some consecutive time stamps *i*:

$$\vec{X}_i = \left[egin{array}{c} x_i \\ y_i \end{array}
ight]$$

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$$ec{V}_i = \left[egin{array}{c} v_{x_i} \ v_{y_i} \end{array}
ight]$$

An example of such observations is given on figure 1 for which aircraft observation ¹⁸⁷ are represented by the blue arrows.



Figure 1. Radar captures associated with three aircraft. In this example only one time sample is considered.

We thus wish to find the vector field described by a linear equation $(\dot{\vec{X}} = \mathbf{A} \cdot \vec{X} + \vec{B})$ which is best fitted to our observations. To illustrate this aspect, we construct a grid over the airspace (see Figure 2) on which we carry out a regression of a vector field that minimizes the error between the model and the observations. In order to use matrix forms, we rewrite equation 1 as $\mathbf{V} = \mathbf{C} \cdot \mathbf{X}$, introducing the following matrices:

$$\mathbf{X} = \begin{bmatrix} x_1 & x_2 & x_3 & \cdots & x_n \\ y_1 & y_2 & y_3 & \cdots & y_n \\ 1 & 1 & 1 & \cdots & 1 \end{bmatrix}$$
(3)

$$\mathbf{V} = \begin{bmatrix} v_{x_1} & v_{x_2} & v_{x_3} & \cdots & v_{x_n} \\ v_{y_1} & v_{y_2} & v_{y_3} & \cdots & v_{y_n} \end{bmatrix}$$
(4)

$$\mathbf{C} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \\ \mathbf{A} \end{bmatrix} \begin{bmatrix} b_1 \\ b_2 \\ \mathbf{B} \end{bmatrix}$$
(5)

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where $\mathbf{X} \in \mathbb{R}^{3 \times n}$, $\mathbf{V} \in \mathbb{R}^{2 \times n}$, $\mathbf{C} \in \mathbb{R}^{2 \times 3}$, $\mathbf{A} \in \mathbb{R}^{2 \times 2}$, $\vec{B} \in \mathbb{R}^{2 \times 1}$ and *n* represents the number of observations at a given instant (number of aircraft present in a sector at a given instant).



Figure 2. Vector field produced by the linear dynamic system

3.2. Regression

The dynamical system has to be adjusted with the minimum error based on the aircraft observations (positions and speed vectors). This fitting has been done with a Least Mean Square minimization (LMS) method[14]. For each considered aircraft *i*, it is supposed that position $\vec{X}_i = [x_i, y_i]^T$ and speed vector $\vec{V}_i = [v_{x_i}, v_{y_i}]^T$ are given. We then construct an error criterion *E*, between the dynamical system model and the observation, based on a norm (Euclidean, in our case), which should be minimized in relation to matrix **A** and vector \vec{B} , and therefore in relation to matrix **C**, which represents the parameters of the model:

$$E = \sqrt{\sum_{i=0}^{i=n} \left\| \vec{V}_i - \left(\mathbf{A} \cdot \vec{X}_i + \vec{B} \right) \right\|^2}$$
$$= \sqrt{\sum_{i=0}^{i=n} \left\| \vec{V}_i - \left(\mathbf{C} \cdot \vec{X}_i \right) \right\|^2}$$
(6)

In a matrix form:

E is minimum w

$$E = \|\mathbf{V} - \mathbf{C} \cdot \mathbf{X}\|$$

E minimization is the same as E^2 minimization: $E^2 = \|\mathbf{V} - \mathbf{C} \cdot \mathbf{X}\|^2$. The derivative of such expression with respect to **C** is given by:

$$\nabla_{\mathbf{C}} E^2 = -2.(\mathbf{V} - \mathbf{C} \cdot \mathbf{X}).\mathbf{X}^T$$

hen: $\nabla_{\mathbf{C}} \mathbf{E} = 0 \Rightarrow \mathbf{C} \cdot \mathbf{X} \cdot \mathbf{X}^T = \mathbf{V} \cdot \mathbf{X}^T$ then:

$$\mathbf{C}_{ont} = \mathbf{V} \cdot \mathbf{X}^T \cdot (\mathbf{X} \cdot \mathbf{X}^T)^{-1}$$

On the right side, we recognize the pseudo-inverse of matrix \mathbf{X}^{T} :

$$\mathbf{X}^+ = \mathbf{X}^T \cdot (\mathbf{X} \cdot \mathbf{X}^T)^{-1}$$

In some situations, $\mathbf{X} \cdot \mathbf{X}^T$ is not invertible, and the computation of the \mathbf{C}_{opt} is not possible by using such equation. In this case, the classical Singular Value Decomposition (SVD) trick is applied:

$$\mathbf{X}^T \cdot (\mathbf{X} \cdot \mathbf{X}^T)^{-1} = \mathbf{L}^T \cdot \mathbf{S}^{-1} \cdot \mathbf{R}$$

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where **S** is a diagonal matrix containing the singular values (only the significant singular values are inverted in this formula in order to control the conditioning of the algorithm). 215

$$\Rightarrow \mathbf{C}_{ovt} = \mathbf{V} \cdot \mathbf{L}^T \cdot \mathbf{S}^{-1} \cdot \mathbf{R}$$

Based on **C** the matrix **A** is extracted for which an eigenvalue decomposition is computed:

$$\mathbf{A} = \mathbf{U} \cdot \mathbf{D} \cdot \mathbf{U}^{T}$$

The diagonal matrix **D** contains the eigenvalues. When such eigenvalues have positive real parts, the system is in expansion mode, and when they are negative, the system is in contraction mode.

In addition the vector \vec{B} represents the global tendency of the vector field.

3.3. Properties of Eigenvalues

The eigenvalues of matrix **A** describe and summarize the evolution of the system. 223 These eigenvalues are complex numbers. Their real parts are related to the convergence 224 or the divergence property of the system in the direction of the eigenvector. When such eigenvalues have positive real parts, the system is in expansion mode (produces divergence), 226 and when they are negative, the system is in contraction mode (produces convergence). 227 The absolute value of these real parts is proportional to the level of contraction or expansion 228 of the system: the larger those real parts are in absolute value, the faster the evolution. 229 Furthermore, the imaginary part of the eigenvalues is related to the level of rotation 230 tendency of the system: the tendency of the system to organize itself following a global 231 rotation movement associated with each of the eigen axes. Depending on those eigenvalues, 232 a dynamical system can evolve in contraction, expansion, rotation, or a combination of 233 those three modes. 234

Then, the evolution properties of the system related to the position of the eigenvalues can be summarized in the complex coordinate system (see Figure 3). In this coordinate system, it is then possible to identify the locus of the eigenvalues of matrix **A** associated with organized traffic situations: the vertical strip around the imaginary axis. Therefore, organized situations are located around the imaginary axis: when the relative distances between aircraft change slowly with time (this means that the relative speeds between aircraft are close to zero and the traffic has no interaction).

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Figure 3. Impact of the eigenvalues of matrix A on the dynamics of the system

As an example (see Figure 4), the eigenvalues of matrix **A** have been calculated for a situation with three aircraft located on a circumference, for which only the orientation of the speed vectors is modified in order to create four traffic situations (pure translation, convergence, divergence, and pure rotation). As we can see in Figure 4, the pure translation and pure rotation are the two organized traffic situations since they have eigenvalues in the central band of the complex plane.



Figure 4. Eigenvalues loci for 4 traffic situations

In the first case, the eigenvalues $\vec{\lambda}$ are null because the aircraft are flying in parallel, 252 representing a translation: distances between aircraft remain unchanged with time. In 253 the second case, the eigenvalues are real negative; the system evolves in a contraction 254 mode, and the four aircraft are converging: the norms of the relative distances between 255 aircraft diminish with time. The third situation represents an expansion evolution for 256 which the eigenvalues are real positive, and the aircraft are diverging: the relative distances 257 increase with time. In the two previous situations, the distance between aircraft changes 258 with time, not being organized traffic patterns. The last situation is associated with full 259 imaginary eigenvalues for which the aircraft stay at the same distance from each other in a 260 curl moving. The computation of matrices **A**, vectors \vec{B} , and $\vec{\lambda}$ is given for these previous examples:

Translation	Convergence	Divergence	Rotation	
$\mathbf{A} = \left[\begin{array}{cc} 0 & 0 \\ 0 & 0 \end{array} \right]$	$\mathbf{A} = \frac{v}{d} \cdot \begin{bmatrix} -1 & 0\\ 0 & -1 \end{bmatrix}$	$\mathbf{A} = \frac{v}{d} \cdot \left[\begin{array}{cc} 1 & 0 \\ 0 & 1 \end{array} \right]$	$\mathbf{A} = \frac{v}{d} \cdot \begin{bmatrix} 0 & 1\\ -1 & 0 \end{bmatrix}$	
$\vec{B} = \begin{bmatrix} v \\ 0 \end{bmatrix}^{-1}$	$\vec{B} = \begin{bmatrix} 0\\0 \end{bmatrix}$	$\vec{B} = \begin{bmatrix} 0\\0 \end{bmatrix}$	$\vec{B} = \begin{bmatrix} 0\\0 \end{bmatrix}$	(7)
$\vec{\lambda} = \frac{v}{d} \cdot \begin{bmatrix} 0 \\ 0 \end{bmatrix}$	$\vec{\lambda} = \frac{v}{d} \cdot \begin{bmatrix} -\vec{1} \\ -1 \end{bmatrix}$	$\vec{\lambda} = \frac{v}{d} \cdot \begin{bmatrix} +\vec{1} \\ +1 \end{bmatrix}$	$\vec{\lambda} = \frac{v}{d} \cdot \begin{bmatrix} +\bar{j} \\ -j \end{bmatrix}$	

Looking at Figure 4, the small squares are the initial positions of aircraft at a given time (this represents the observation given by radar, for instance, with the associated speed vector). As it can be seen, the aircraft are initially located on a circumference with a diameter of $2 \cdot d$. The positions of aircraft two and three are symmetric to the x-axis. All the speed norms are the same and have been fixed at v. The vector field associated with each one of these four situations is shown in Figure 5.



Figure 5. Vector field produced for the 4 toy examples. The red arrows represent the vector filed of the associated linear dynamical system model.

3.4. Extension with uncertainties

If we want to predict complexity in a given airspace, one must be able to take into 270 account future aircraft positions uncertainties which are crossing such airspace. Those 271 uncertainties are linked to the wind and temperature encountered by the aircraft along its 272 route. So, future positions of aircraft will be represented by a segment along its trajectory 273 arc length in the future. Therefore, since we should account for these uncertainties, it has 274 been considered that at every sample time of the analysis, each aircraft that is within the 275 current modeled airspace area can be ahead or behind its actual position. Then, a time 276 shift is applied to each aircraft (i.e., the reference one and the neighbors) to account for ten 277 forward and ten backward positions. Each shift is equal to twelve seconds, so the most 278 forward and backward positions are separated two minutes with respect to the reference 279 position. 280

In order to simplify the following figures, we will consider only two shifts in each direction (five positions in total per aircraft) instead of ten only for the visualization of the uncertainties problem in this current section. In Figure 6, the three aircraft from Figure 1 are expanded with their corresponding forward and backward positions after applying a time-shifting.



Figure 6. Uncertainties associated with three aircraft

Figure 7 shows the vector field produced by the linear dynamical system corresponding to the above situation. 287



Figure 7. Vector field of the uncertainties extension



Figure 8 compares the vector field of the situation with and without the uncertainties 288 extension. 289



(a) Real traffic situation

(b) Extension with uncertainties



This extension will make matrix X larger since from here on, n would be equal to $5 \cdot number \ of \ aircraft.$

3.5. Metric computation

Having obtained matrix **A** and its eigenvalues, the metric is built by summing the negative real part of such eigenvalues λ hereinafter. 299

Therefore, the procedure that we apply consists of solving the LMS method while 300 following an aircraft along all the position observations of its trajectory. This aircraft will be 301 referred to as the reference aircraft. As for the aircraft that are flying in its vicinity, they will 302 be referred to as neighbor aircraft. Every aircraft within the searching area of the reference 303 aircraft at each time will be considered as a neighbor aircraft, and therefore, its observations 304 will be used in the *LMS* computation (at each time, the neighbor aircraft may be different). 305 This searching area is defined as a box window (24.8 x 24.8 NM) centered at each reference 306 aircraft position. This dimension is based on the longitudinal separation minima applicable 307 to en-route aircraft multiplied by a scalar factor. 308

The uncertainty extension will be applied to both reference and neighbor aircraft. So matrix **A** is computed using the observations of the reference and neighbor aircraft and their uncertainties as well, at each time. Figure 9 shows the geometry of the problem that is solved for a reference aircraft at a given time.



Figure 9. Example of local trajectory interaction at a given time

3.6. Neighborhood definition

In order to reflect operational features, the metric has been extended to the third dimension by using three-dimensional state space. From the operational point of view, what is relevant for air traffic controllers is the horizontal speed of the aircraft and their climbing/descending rate. So, the model has been extended in this direction by considering only some aircraft in the neighborhood of a given aircraft.

When the reference aircraft is climbing or descending, all the other aircraft in the 319 neighborhood will be considered as neighbors. For a cruising reference aircraft, one must 320 apply filtering to account for aircraft that are flying in the same flight level; however, an 321 extension of this filter was necessary to account for the aircraft that were changing their 322 altitude and then were likely to interact with other aircraft since they would be flying at 323 the same altitude at some point of the analysis period. The criteria applied to both the 324 reference and neighbor aircraft to filter the possible aircraft affecting the local disorder can 325 be seen in Figure 10. 326



Figure 10. Aircraft altitude evolution that has an interaction with a certain FL

When the neighbor aircraft altitude (after applying the searching area principle) is close to the reference aircraft altitude, that neighbor aircraft is considered as an actual 328 neighbor aircraft. In RVSM (Reduced Vertical Separation Minima) airspace, en-route aircraft vertical separation is 1000 *ft* between FL290 and FL410. The filter is set to look 330 for neighbor aircraft within a vertical separation, with respect to the reference one, equal 331 to 3000 ft. Therefore, aircraft flying within 30 flight levels above and below the reference 332 aircraft will be considered for the metric. The filter allows the following situations for both 333 the reference and neighbor aircraft: (*a*) aircraft is climbing to the reference aircraft altitude, 334 (b) aircraft is descending to reference aircraft altitude, (c) aircraft is about to climb from 335

reference aircraft altitude, (d) aircraft is about to descend from reference aircraft altitude, (e) aircraft is climbing and will fly from a lower to a higher altitude than reference aircraft 337 altitude, (f) aircraft is at reference aircraft altitude, (g) aircraft is descending and will fly 338 from a higher to a lower altitude than reference aircraft altitude. 339

When two cruising aircraft are flying at different altitudes (see the example given in 340 Figure 11), such aircraft will never be considered as neighbors because they will always 341 stay separated thanks to the vertical separation. 342



Figure 11. Lack of interdependency between two consecutive flight level trajectories

After filtering the neighboring aircraft associated with a reference aircraft (at a given 343 time *t*), the LMS computation is applied in order to identify the A matrix. The metric is 344 then computed based on the eigenvalues of such A matrix and assigned to the reference 345 aircraft at time t. This computation is done for each trajectory sample along the route. 346

Having this complexity metric computed along the trajectory, it is possible to establish 347 a color map that shows the aircraft involved in congested areas. 348

4. Results

4.1. Toy Examples

Different traffic samples have been created in order to compare the complexity metric 351 previously described. For the following toy examples, no uncertainties are considered 352 and every aircraft is flying at the same flight level. Six traffic situations will be classed 353 according to an increasing level of difficulty (increasing order of complexity) as a function 354 of predictability and interdependency between trajectories. The full trajectories of aircraft 355 are shown in the following figures, where a green circle symbolizes their initial positions. Figure 12 shows a parallel flow of aircraft. It represents an easy situation since aircraft 357 relative distances keep the same and in this case this is no complexity (null A matrix; see 358 equation 7). 359



Figure 12. Parallel flow

Figure 13(a) shows a full symmetric convergence of eight aircraft flying at the same 360 speed. It represents an average situation with high sensitivity and conflicts with no 361 interaction between solutions. In order to build an aggregated metric along the time 362 dimension, we compute for each time sample the associated eigenvalues of the A matrix 363 for which the real parts are summed up in order to produce a scalar value (Figure 13(b)). 364 It must be noticed that the metric begins to be negative, showing the situation is globally 365

converging. If we continue evaluating that situation along time, after the crossing of the aircraft, the metric becomes positive, and the situation is globally diverging.





(**a**) Eight aircraft converging at the same point.

(b) Evolution of the real part of A matrix eigenvalues.

Figure 13. Scalar metric function of time for eight aircraft converging at the same point. As it is shown there is a discontinuity when aircraft cross each other but if we consider more aircraft in the crossing, the curve will be scaled accordingly (more aircraft will induce larger negative and positive values).

Figure 14(a) shows a fuzzy convergence of aircraft in the same area. Aircraft do not necessarily have the same speed.





(**a**) Random aircraft converging in the same area.

(b) Scalar metric for random aircraft converging in the same area.

Figure 14. Complexity evolution with time associated to the fuzzy convergence situation.

In this case, the metric first identifies a soft converging pattern. Then, it reaches a minimum in the central area of convergence (matching the maximum convergence tendency) and begins to be positive, meaning that the aircraft are diverging at that moment (see Figure 14(b)) and then reaches its maximum (matching the maximum divergence tendency).

We then consider two flow crossing situations. The first situation has a crossing angle of 30 degrees (see Figure 15), and the second one has a crossing angle of 90 degrees (see Figure 16). The right side of both figures represents the evolution of the complexity metric with time. As expected, the metric stat is to be negative as the aircraft start first to converge and become positive (divergence) after the crossing point. The shapes of the curve are the 370 same. Only the magnitude is higher with the 90 deg situation, which is expected since the relative speed between aircraft is higher in this situation. 381



Figure 15. N-S and W-E flows crossing at 30 deg. Traffic situation on the left, complexity function of time on the right.



Figure 16. N-S and W-E flows crossing at 90 deg. Traffic situation on the left, complexity function of time on the right.

It is worth mentioning that in these three cases. However, each aircraft possesses a different speed. The eigenvalues are always real: the no-curl tendency is perceived since the set of aircraft is flying only along two different trajectory directions. 382

4.2. Real Airspace

This complexity metric has been computed on traffic simulated with real flight plans 386 of aircraft crossing the French airspace (as a matter of fact, using real traffic data like radar 387 tracking records is meaningless because such traffic has been managed by the controller and 388 complexity has been removed). Based on such flight plans, an arithmetic simulator based 389 on the BADA database has been used in order to create 8000 four-dimensional trajectories 390 in the french airspace. The trajectory has then been sampled every 20 seconds, representing 391 two million 4D points for the whole day. The metric has been computed for each trajectory 392 and for each time step in a 4D cube (three spatial dimensions and one time dimension) and 393 projected on a two-dimensional coordinate system to have a complexity map as shown 394 in Figure 17. On this figure, the metric has been normalized between 0 (blue color) and 305 100% (maximum with red color). As expected, the highest complexity is located near the 396

big crossings. One must remember that the map represents the accumulated complexity in altitude and time. A 2D point at (x,y) on the map represents all 4D points at those 2D coordinates (x,y).

The metric has been implemented in Java. Thanks to some algorithmic improvements, the computation time needed to compute the metric for the whole day of traffic (two million points) is less than ten milliseconds on a core i7 Laptop computer.



Figure 17. Traffic complexity of a traffic sample over French airspace. For each 4D point (x,y,z,t) of each trajectory, the complexity metric is computed and represented with a color map on a two dimension map (x,y).

5. Conclusion

This paper has introduced an efficient traffic complexity metric that can identify the 404 level of disorder of a given traffic situation. A Linear Dynamical System model is first 405 regressed based on a least mean square approach based on a set of trajectory samples. An 406 SVD trick has been used in order to avoid conditioning issues in the LMS process. Then, 407 the eigenvalues of the associated **A** matrix of the linear dynamical system are extracted to 408 quantify the disorder of the traffic situation (sum of the negative real parts). When such a 409 metric has to be computed for a predicted traffic situation, one must be able to take into 410 account uncertainties. This uncertainty has been taken into account by considering aircraft 411 as segments in the time dimension in order to produce a robust metric. This metric has 412 been successfully tested on several artificial traffic situations and on a full day of traffic 413 over the french airspace. Based on the high performance for computing this metric (for a 414 large number of trajectories), the next step consists of using this metric in an optimization 415 algorithm to minimize congestion in a given airspace, which is one of the objectives of the 416 START SESAR project. 417

Author Contributions: Conceptualization, D.D, A.G, S.C and M.S; methodology, D.D, A.G, J.L, S.C	
and M.S; software, D.D, A.G and J.L; validation, D.D, A.G, J.L, S.C and M.S	419
Funding: The SESAR START project has founded the research (grant number 893204).	420
Conflicts of Interest: The authors declare no conflict of interest.	421
Sample Availability: Samples of the compounds are available from the authors.	422

Abbreviations

The follo	wing abbreviations are used in this manuscript:
ATC	Air Traffic Control
ATM	Air Traffic Management
BADA	Base of Aircraft DAta
COVID	COrona VIrus Disease
FIR	Flight Information Region
LMS	Least Mean Square
NASA	National Aeronautics and Space Administration
NM	Nautical Mile
RVSM	Reduced Vertical Separation Minima
SESAR	Single European Sky's ATM Research
START	Stable and resilienT ATM by integrAting Robust airline operations into the neTwork
SVD	Singular Value Decomposition

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